ECEN 689 High-Speed Links Circuits and Systems

Lab4 – Receiver Circuits

Objective
To learn fundamentals of receiver circuits.

Introduction
Receivers are used to recover the data stream transmitted by transmitters. The voltage and time domain resolution and offset are the key performance specs for receiver circuits. In this lab, the receiver building blocks will be studied and practiced. Their performance metrics are going to be characterized.

Receiver Parameters
A receiver’s performance is measured in both time and voltage domain. How small voltage a receiver can measure is the sensitivity. The receiver’s voltage offset is the similar concept as a comparator’s input offset voltage, which is caused by the device mismatch and circuit structure. In time domain, the shortest pulse width the receiver can detect is called the aperture time. It limits the maximum data rate of the link system. The time offset becomes the timing skew and jitter between the receiver and some reference timing marker (CDR). These four parameters are illustrated in Figure 1.

Figure 1 Eye Diagram Showing Time and Voltage Offset and Resolution [Dally]

Basic Receiver Block Diagram
Pre-amplifier is often used in the receiver side to improve signal gain and reduce input referred noise. It must provide gain at high frequency bandwidth so that it does not attenuate high frequency data. It can also operate as a common mode shifter to correct the common mode
mismatch between TX and RX. Offset correction can also be implemented in the pre-amplifier. The comparator/sampler can be implemented with static amplifiers or clocked regenerative amplifiers. If the power consumption is a concern, clocked regenerative amplifier is preferred.

Figure 2 Basic Receiver Block Diagram

Clocked Comparators

Clocked comparators can sample the input signals at clock edges and resolves the differential. They are also called regenerative amplifier, sense-amplifier, or latch. Two clocked comparators are shown in Figure 3. A flip-flop can be made of cascading an R-S latch after strong-arm as shown in Figure 4. It also can be formed by cascading two CML latches.

Figure 3 Clocked Comparators (a) Strong-Arm Latch (b) CML Latch

Figure 4 Flip-Flop made of a Strong-Arm Comparator and an RS Latch
Clocked Comparator LTV Model and ISF

A comparator can be viewed as a noisy nonlinear filter followed by an ideal sampler and slicer (comparator) as shown in Figure 5 [2]. The small-signal comparator response can be modeled with an ISF of

$$\Gamma(\tau) = h(t, \tau) \quad (1)$$

The comparator ISF is a subset of a time-varying impulse response $h(t, \tau)$ for LTV system, which can be expressed as

$$y(t) = \int_{-\infty}^{\infty} h(t, \tau)x(\tau)d\tau \quad (2)$$

where $h(t, \tau)$ is the system response at $t$ to a unit impulse arriving at $\tau$ and for LTI system $h(t, \tau) = h(t-\tau)$ using convolution. Output voltage of comparator can be expressed as

$$V_o(t_{obs}) = \int_{-\infty}^{\infty} V_i(\tau)\Gamma(\tau)d\tau \quad (3)$$

and the comparator decision can be calculated as

$$D_K = sgn(V_K) = sgn(V_o(t_{obs} + KT)) = sgn\left(\int_{-\infty}^{\infty} V_i(\tau)\Gamma(\tau)d\tau\right) \quad (4)$$

Please refer to [2] for details.

Characterizing Comparator ISF using Cadence

The characterization of a comparator’s ISF can be found in [2]. The simulation block diagram is shown in Figure 6. A small step signal is applied to the comparator at time $\tau$ with a small offset voltage. The offset voltage is generated through a simple servo loop, which makes the comparator metastable. The $V_{\text{metastable}}$ is measured for various time $\tau$ to obtain the step sensitivity.
function SSF ($\tau$). Cadence simulation setup is shown in Figure 7. Both input step and clock signals are set to be the same frequency and with time $\tau$ delay. At the metastable condition, the flip-flop generates equal number of 1s and 0s. The percentage of 1s and 0s controls the average current flow direction of the voltage control current source (VCCS) which generates an offset voltage on the shunt capacitor. The simulation can be done by sweeping the time $\tau$ and measure the offset voltage. ISF can be eventually generated from those simulation results [2]. Please also refer to the appendix in this lab.

Figure 6 Characterization of Comparator ISF [Jeeradit VLSI 2008]

Figure 7 Cadence Comparator ISF Setup
Pre-Lab

1. Generally circuits are designed to handle a minimum variation range of ±3α. What is the yield rate for ±α, ±2α, ±3α, and ±4α?

2. A Comparator’s input referred offset is primarily a function of the input transistor pair’s threshold voltage V\text{th} mismatch and a weaker function of β (mobility) mismatch. Assuming the mismatch is dominated by the threshold voltage, please estimate the transistor width to have input referred offset σ = 5.11mV with L=100nm. For our default 90nm technology A\text{VT} is 2.8mV\text{um}. The result can be used for the comparator design.

\[
\sigma_V = \frac{A_{VT}}{\sqrt{WL}}
\]  \hspace{1cm} (5)

3. Demultiplexer is often used to deserialize a stream of high speed data. It can be implemented after the receiver circuit to generate lower speed data. Please design a 1:2 De MUX that deserializes 4Gb/s data into 2Gb/s data. Figure 9 is an example of 1:2 De-MUX, please refer to [3] as a reference. Please use behavioral models to implement the De-Mux and show your simulation results.
Questions

1. High-Speed Comparator Design. This problem involves the design of 4 different high-speed comparators to meet the following specifications:
   a. \( \text{clk} \rightarrow \text{Dout} \text{ delay} \leq 200\text{ps} \) with a 10mV static differential input voltage (Din+\(-\text{Din}-\)) at a common mode voltage of 80\(^\%\)*VDD. Measure delay from when the clock is at 50\(^\%\) VDD to Dout+ is at 50\(^\%\) VDD for an output rising transition. Please refer to Figure 18.
   b. Clock frequency = 2GHz. Use at least one inverter-based buffer to clock your circuit for realistic clock waveforms.
   c. Load cap on Dout+ and Dout- is 10fF.
   d. Input referred offset \( \leq 10\text{mV} \). Here you can optimistically assume that the input referred offset is just due to the input differential pair Vt mismatch and use the mismatch equation given in the notes, i.e. no need to run Monte Carlo simulations.
   e. Optimize the design for power consumption, i.e. don’t overdesign for a supper small delay. Try to minimize total capacitance while still meeting the 200ps delay and offset specifications.

**Design the comparators based on the following 4 architectures:**

a. **Conventional Strong-Arm Latch.** For an example schematic, refer to Figure 4 in [4]. Feel free to change the pre-charge transistors configuration if you desire.

b. **CML Latch.** For an example schematic, refer to Figure 11a in [5].

c. **Schinkel Low-Voltage Latch.** For an example schematic, refer to Figure 2 in [6].

d. **Goll Low-Voltage Latch.** For an example schematic, refer to Figure 2 in [7].

**The comparators should realize a flip-flop function.**

a. As shown in Figure 10, for the Strong-Arm type latches (1, 3, and 4) follow with the optimized SR-latch shown in Figure 11. For more details on the optimized SR-latch, refer to [8]

   **Note:** for architecture (3) you will need to modify this optimized SR-latch – as the sense-amp pre-charges to GND (vs VDD in 1 & 4).

b. To realize a CML flip-flop with architecture (2), simply cascade 2 CML latches to realize a master-slave flip-flop.
1. High-Speed Comparator Characterization. Please read [2] and [9]. Please simulate all FOUR comparators and produce the following using 500MHz Clock signal:

   a. **Plot comparator delay vs. VDD** for VDD varying from 50% of nominal VDD to 100% VDD. For this keep the input common mode equal to 80% of the supply, i.e. sweep the input common-mode along with the supply. Also scale the clock input signal level with VDD.

   b. **Plot comparator power vs. VDD** in a similar manner.

   c. **Generate the comparator Impulse Sensitivity Function (ISF) at the nominal VDD, 80% VDD and 60% VDD (3 curves).** Again, track the input common-mode with VDD. To do this use the equivalent test circuit in Slide 9 of Lecture 14, for more details refer to [2] For the characterization try an input differential step input of 50mV,
i.e. VCM±25mV for the differential input signals. **Report the comparator aperture time**, by measuring the 10%-90% “rise-time” from simulation. Please refer to [9] for the aperture time measurement.

d. Please compare the design of these FOUR latches. You can refer to [2]

2. Link Verification. The comparator designed can be considered as a basic receiver. Please build a 4Gb/s link system by using the transmitter designed either in voltage mode or current mode and the comparator which you chosen for the best performance. Please refer to Figure 12. Use 50Ω transmission line with 1ns delay. Add 200fF parasitic caps at the output of your transmitter. Feel free to choose the best termination and coupling schemes.
   a. Please show the circuit schematic including coupling and termination.
   b. Explain why you choose your coupling and termination scheme.
   c. Please show simulation results and eye diagram and verify the link performance.

![Figure 12 Basic Link System using DC Coupling](image-url)
Reference


Appendix

ISF simulation steps:

Figure 13 Transient Simulation of ISF Test Circuit at time $\tau$

Figure 14 Direct Plot of $V_{ms}$ at each time $\tau$ after parametric sweep
Figure 15 $V_{ms}$ vs. time $\tau$ with $V_H=24.3\text{mV}$ and $V_L=-24.3\text{mV}$ through measuring the average voltage of $V_{ms}$ after settling.

Figure 16 Generating SSF from Figure 15.
Finally, the ISF can be plotted through taking the derivative of the Figure 16 as shown in Figure 17.

Figure 17 ISF for SA Latch at 1.2V

To do reasonable CLK to Dout delay measurement
Some point the polarity of (Din+ - Din-) has to be changed.
Ex) Before 0.75ns Din+ - Din- = -10mV, and after 0.75ns Din+ - Din- = 10mV

Figure 18 Clk to Dout Delay Measurement (I)
Figure 19 Clk to Dout Delay Measurement (II)