

ECEN325: Electronics

Spring 2014

Diode Rectifier Circuits



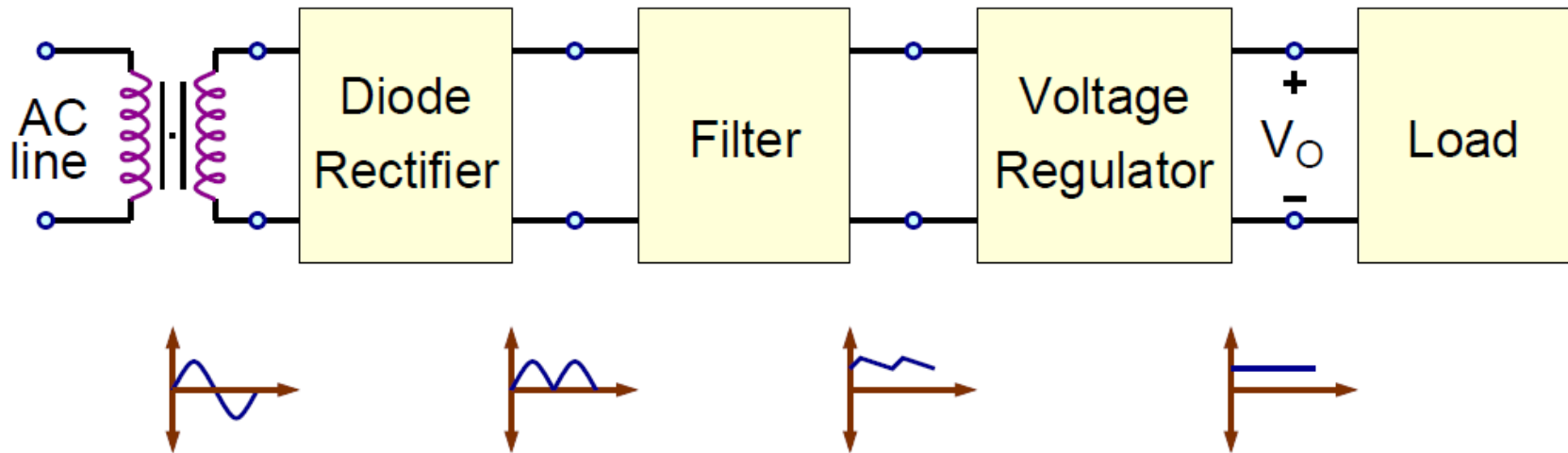
Sam Palermo

Analog & Mixed-Signal Center

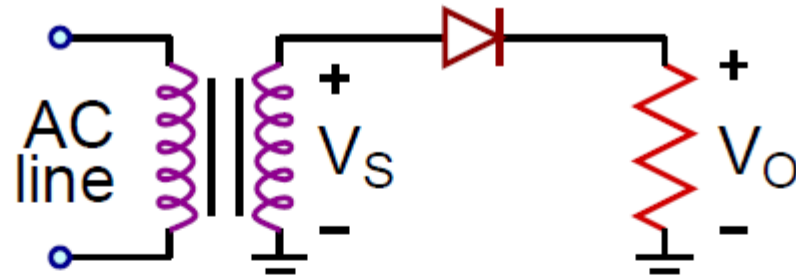
Texas A&M University

Rectifier Circuits

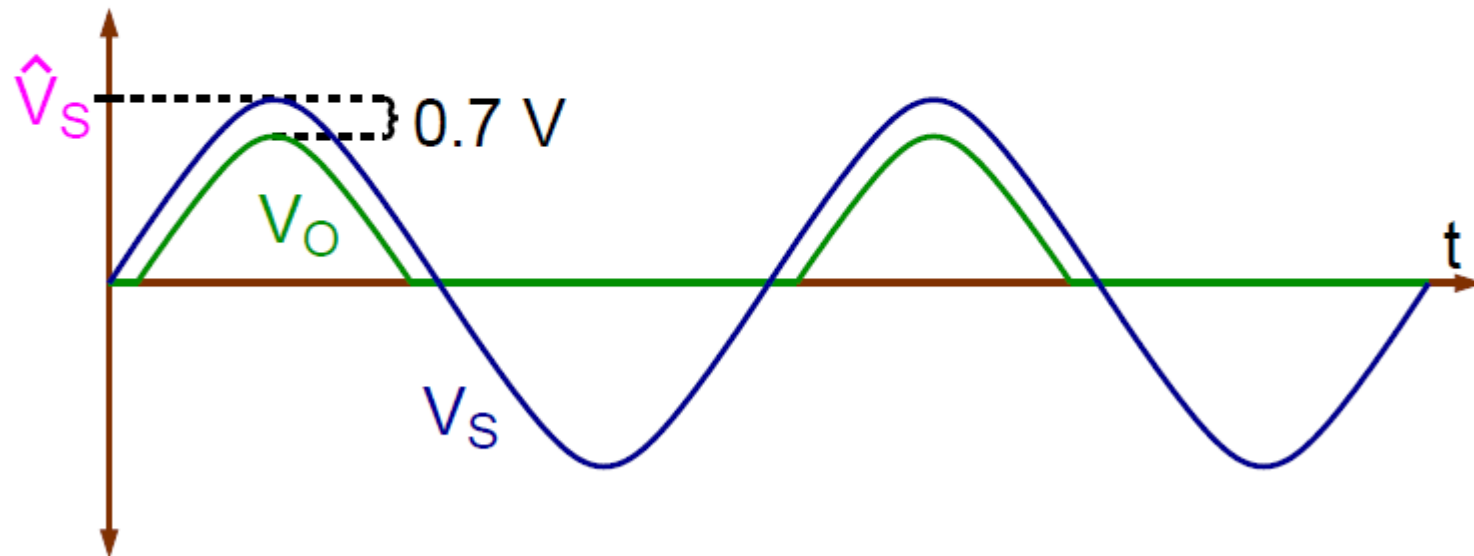
[Karsilayan]



Half-Wave Rectifier



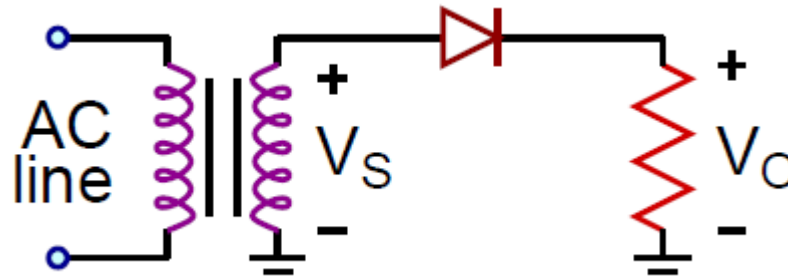
[Karsilayan]



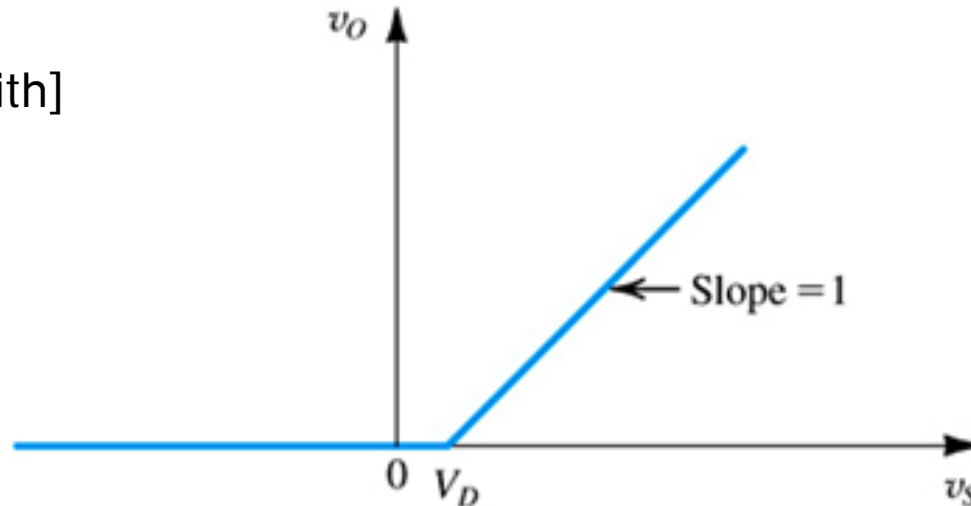
$$PIV = \hat{V}_S$$

Half-Wave Rectifier Transfer Characteristic

[Karsilayan]

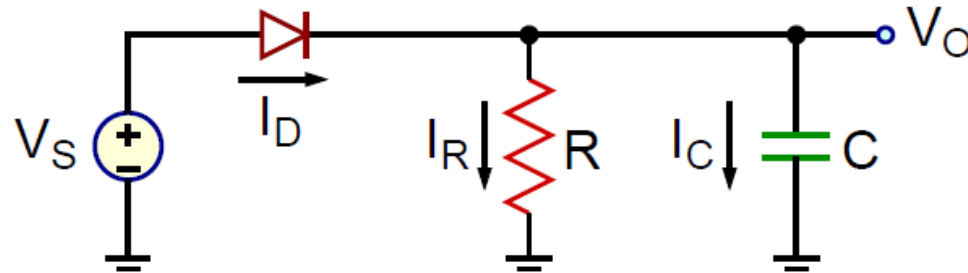


[Sedra/Smith]

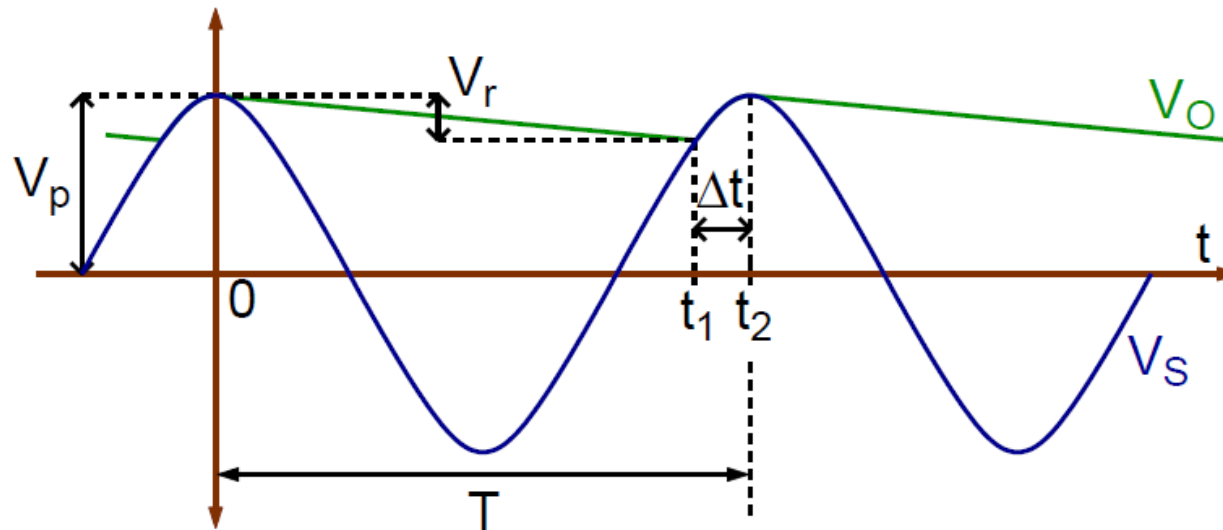


- Only rectifies positive half of the input signal
- Lose one diode voltage drop from the peak value

Half-Wave Rectifier w/ a Filter Cap



[Karsilayan]



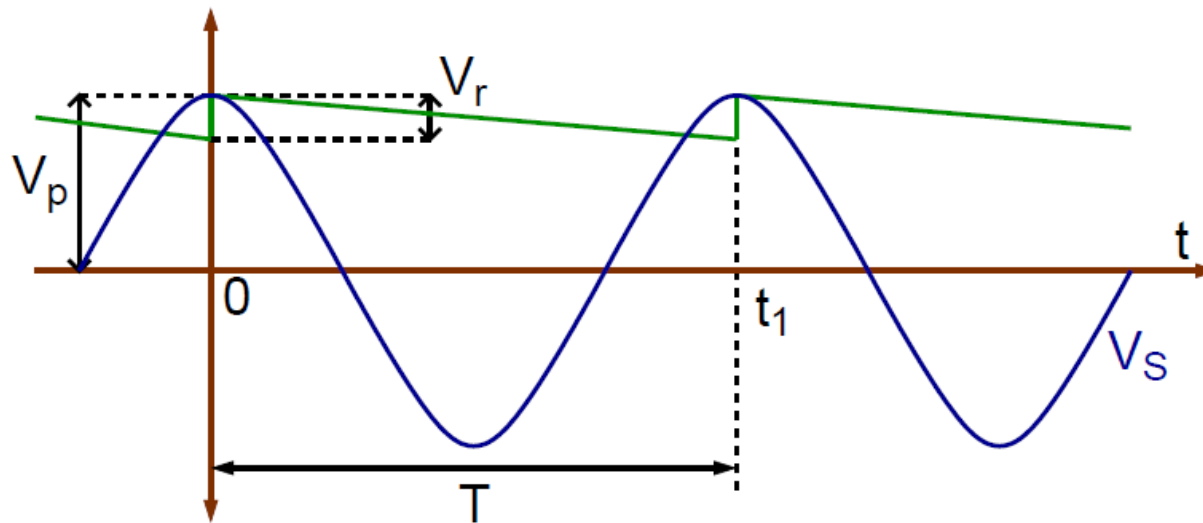
$$V_o(t) = \begin{cases} V_s(t) - 0.7V, & t_1 < t < t_2 \\ V_p e^{-\frac{t}{RC}}, & 0 < t < t_1 \end{cases} \Rightarrow V_o(t_1) = V_p e^{-\frac{t_1}{RC}}$$

Half-Wave Rectifier w/ a Filter Cap

For a properly designed filter:

[Karsilayan]

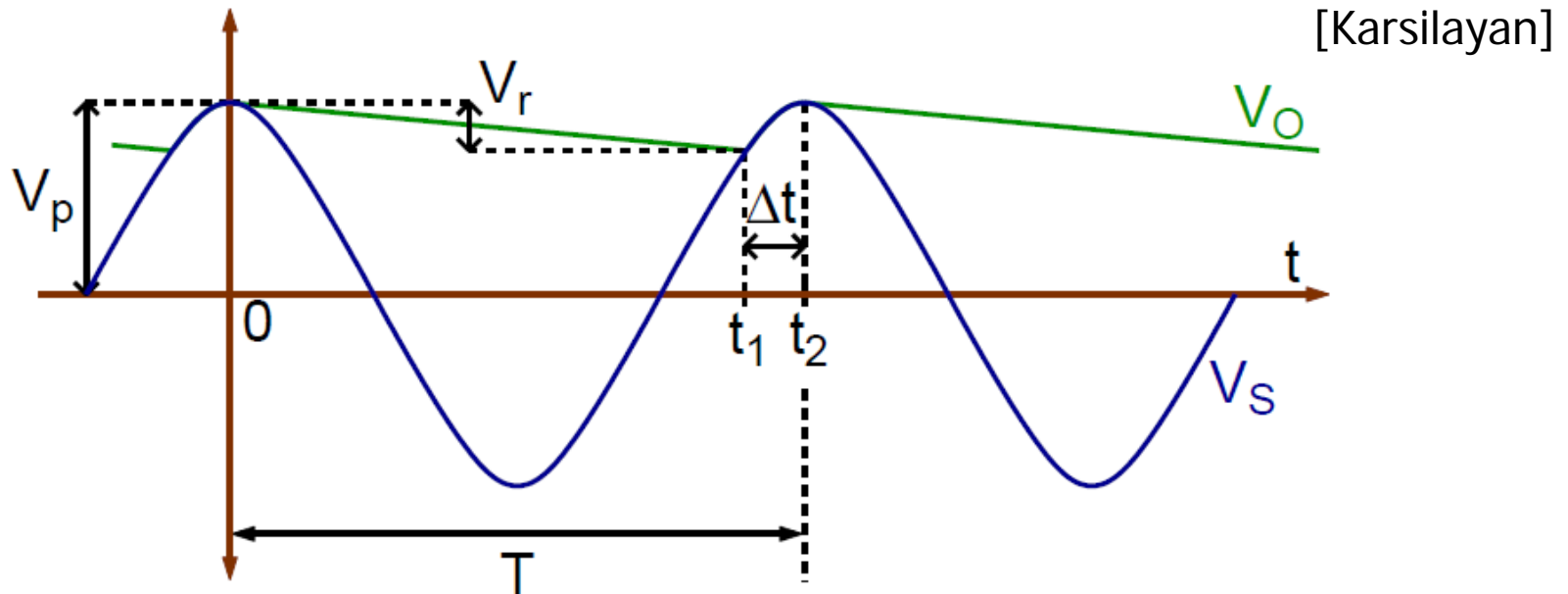
$$\left. \begin{array}{l} t_1 \approx T \Rightarrow V_O(t_1) \approx V_p e^{-\frac{T}{RC}} \\ RC \gg T \Rightarrow e^{-\frac{T}{RC}} \approx 1 - \frac{T}{RC} \end{array} \right\} \Rightarrow V_O(t_1) = V_p \left(1 - \frac{T}{RC} \right)$$



Peak-to-peak ripple voltage:

$$V_r = V_p - V_O(t_1) = V_p - V_p \left(1 - \frac{T}{RC} \right) \Rightarrow V_r = V_p \frac{T}{RC}$$

Half-Wave Rectifier w/ a Filter Cap

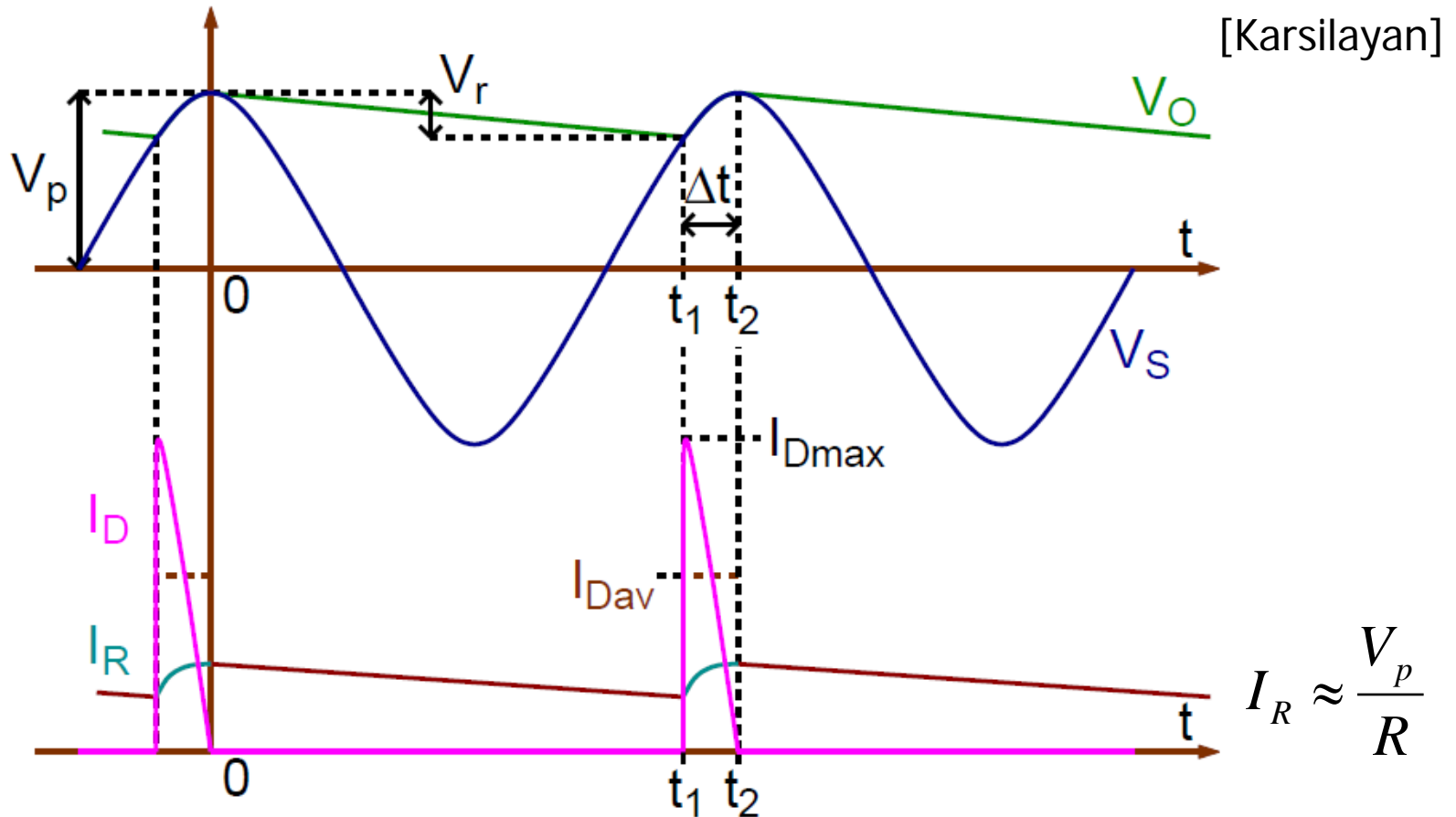


$$V_p \cos(\omega \Delta t) = V_p - V_r$$

$$\omega \Delta t \text{ is small} \Rightarrow \cos(\omega \Delta t) \approx 1 - \frac{1}{2}(\omega \Delta t)^2$$

$$\Rightarrow \omega \Delta t \approx \sqrt{\frac{2V_r}{V_p}} \Rightarrow \Delta t \approx \frac{T}{2\pi} \sqrt{\frac{2V_r}{V_p}}$$

Half-Wave Rectifier w/ a Filter Cap



During conduction (t_1-t_2): $Q_{supplied} = Q_{lost}$
 $I_{Cav}\Delta t = CV_r$

Half-Wave Rectifier w/ a Filter Cap

Substitute Δt in $I_{Cav}\Delta t = CV_r$

[Karsilayan]

$$I_{Cav} \frac{T}{2\pi} \sqrt{\frac{2V_r}{V_p}} = CV_r \Rightarrow I_{Cav} = \frac{2\pi CV_r}{T} \sqrt{\frac{V_p}{2V_r}}$$

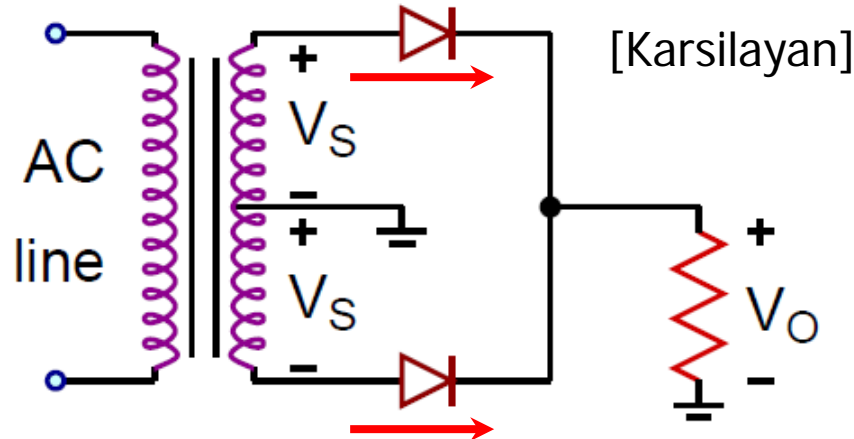
$$I_{Dav} = I_R + I_{Cav} = I_R + \frac{2\pi CV_r}{T} \sqrt{\frac{V_p}{2V_r}}$$

$$V_r = V_p \frac{T}{RC}, \quad V_p \approx I_R R \Rightarrow V_r = I_R \frac{T}{C}$$

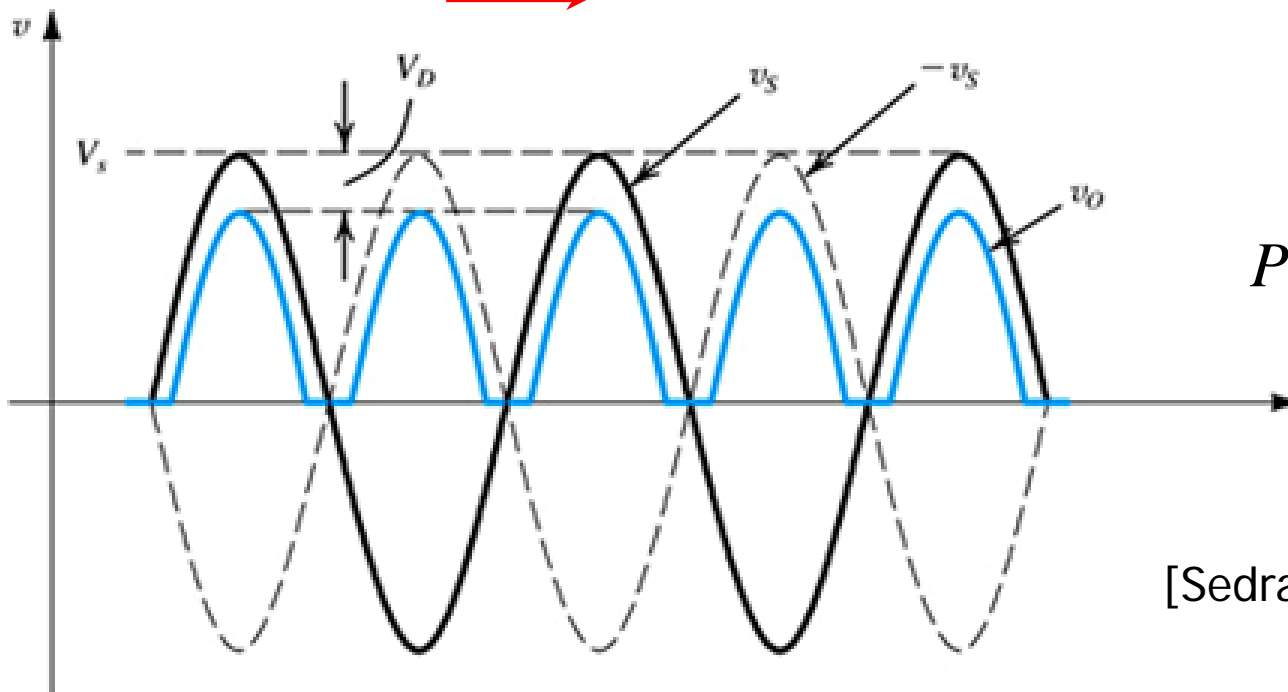
$$I_{Dav} = I_R + 2\pi I_R \sqrt{\frac{V_p}{2V_r}} = I_R \left(1 + \pi \sqrt{\frac{2V_p}{V_r}} \right)$$

$$I_{Dmax} = I_R \left(1 + 2\pi \sqrt{\frac{2V_p}{V_r}} \right) \quad (\text{assuming a triangular capacitive current profile})$$

Full-Wave Rectifier



- Positive ½ cycle
 - Top diode on
- Negative ½ cycle
 - Bottom diode on

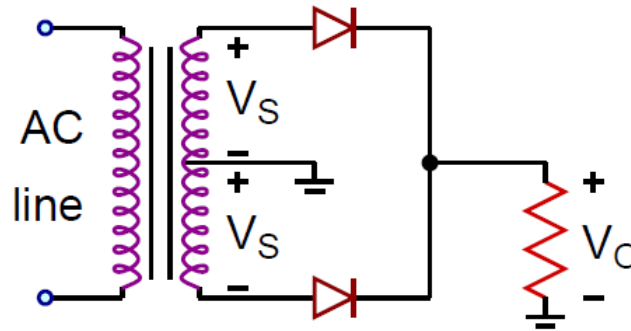


$$PIV = 2\hat{V}_s - 0.7V$$

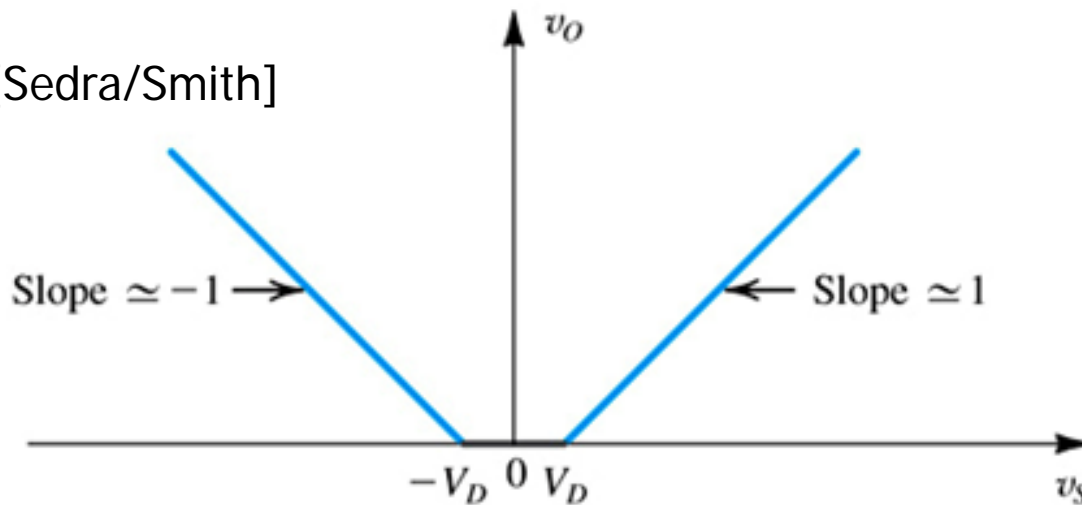
[Sedra/Smith]

Full-Wave Rectifier Transfer Characteristic

[Karsilayan]



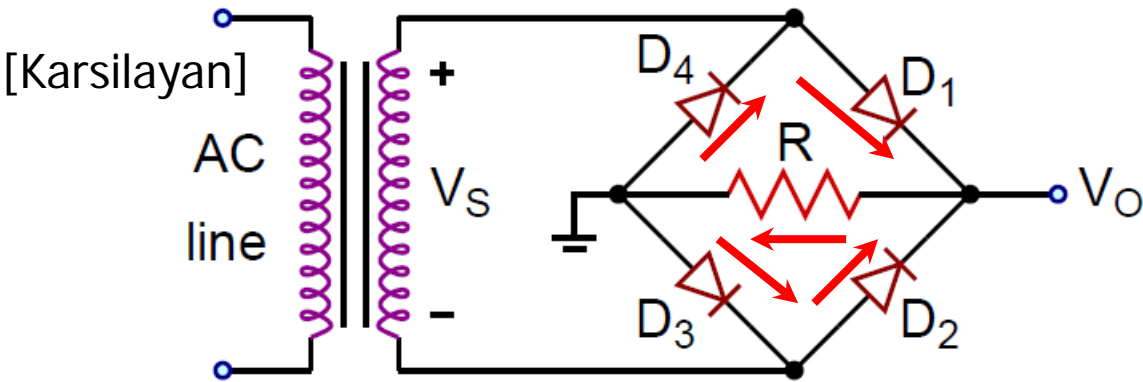
[Sedra/Smith]



- Rectifies all of the input signal
- Lose one diode voltage drop from the peak value

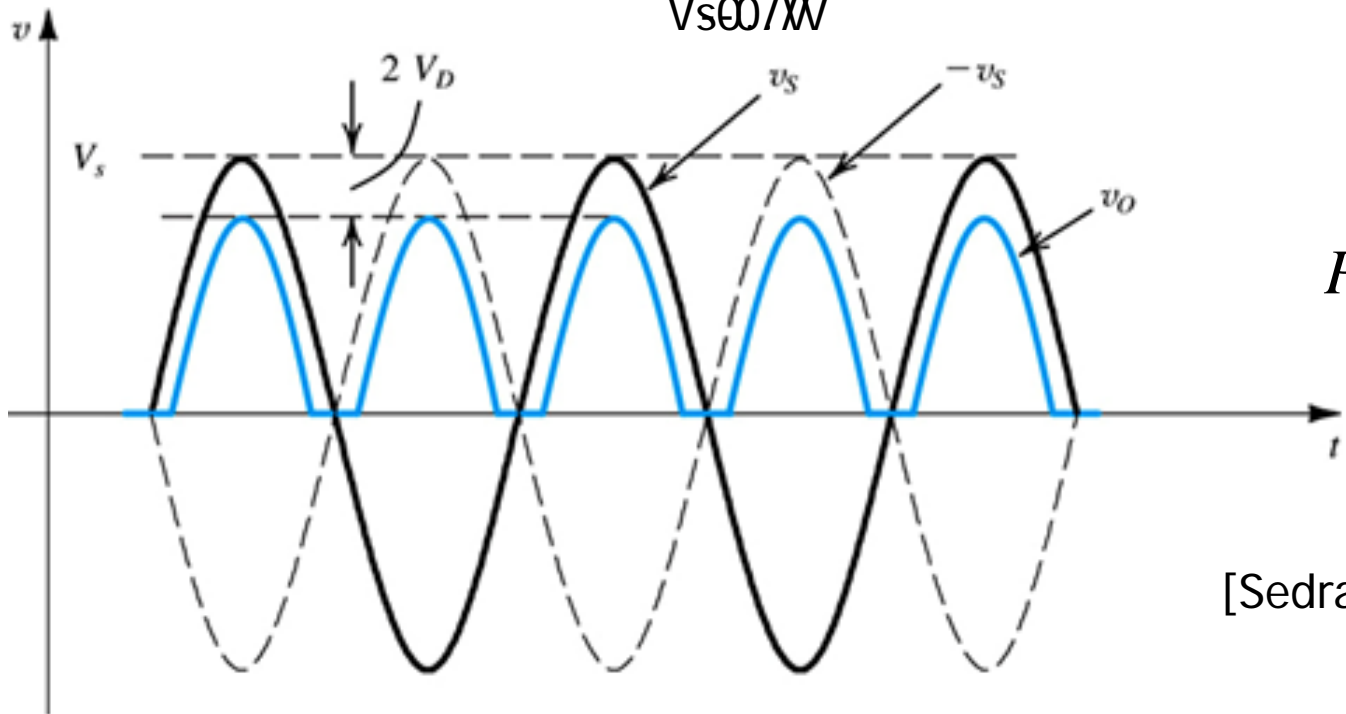
Bridge Rectifier

\ -0.7V



- Positive 1/2 cycle
 - D1 & D3 on
- Negative 1/2 cycle
 - D2 & D4 on

$V_s \sin \omega t$

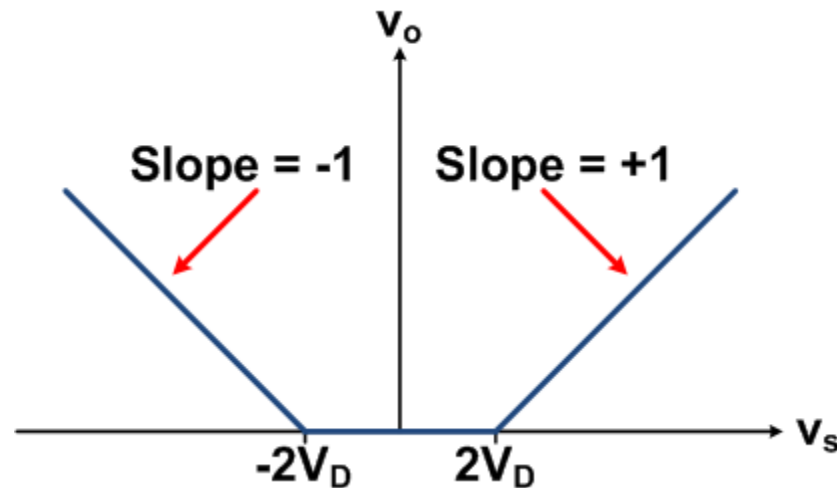
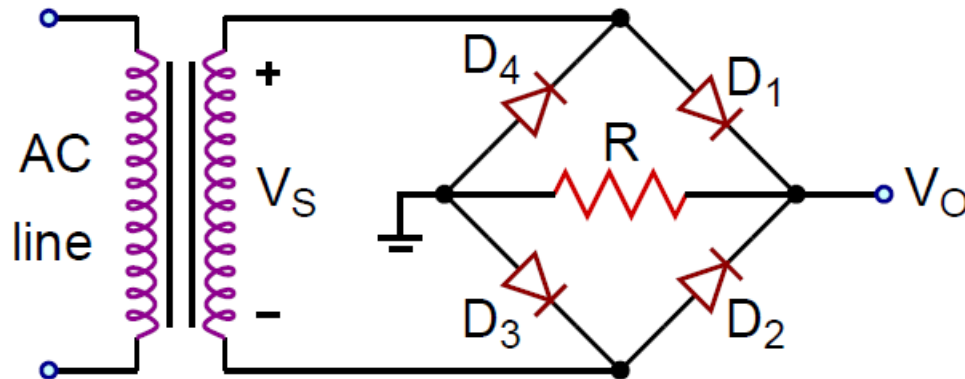


$$PIV = \hat{V}_s - 0.7V$$

[Sedra/Smith]

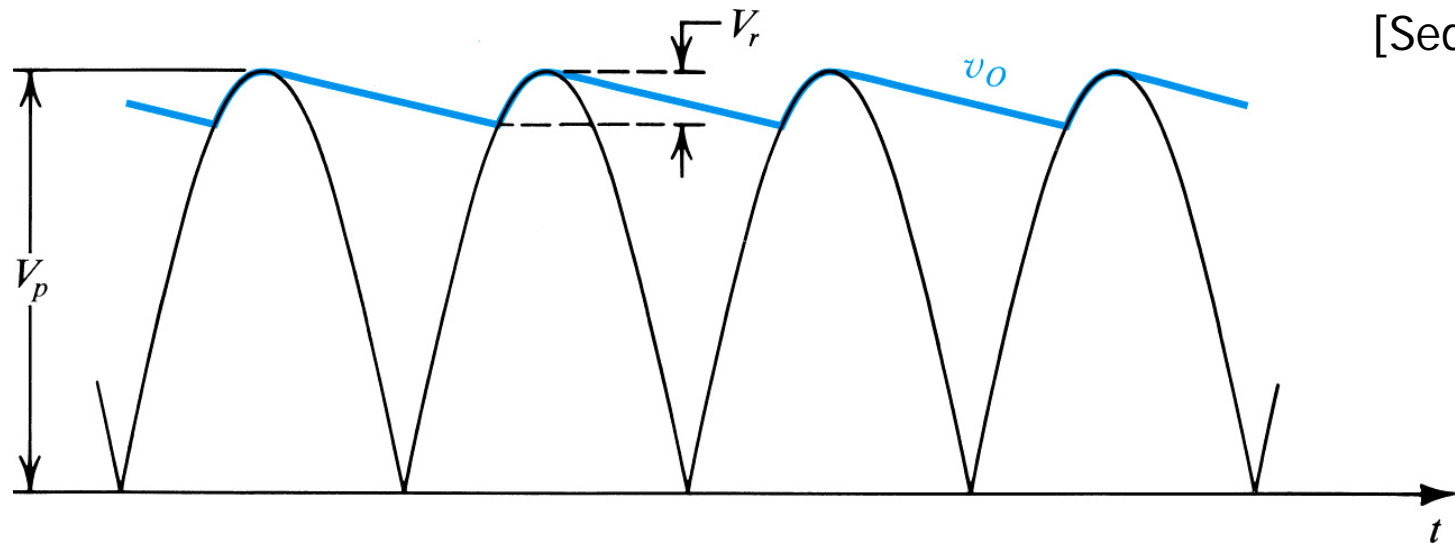
Bridge Rectifier Transfer Characteristic

[Karsilayan]



- Rectifies all of the input signal
- Lose two diode voltage drops from the peak value

Full-Wave & Bridge Rectifier w/ a Filter Cap



[Sedra/Smith]

- The capacitor only discharges for $T/2$
 - Results in $1/2$ Cap size for a given ripple
 - Roughly $1/2$ diode current

$$V_r = V_p \frac{T}{2R_L C_L} \quad I_{Davg} = I_R \left(1 + \pi \sqrt{\frac{V_p}{2V_r}} \right) \quad I_{Dmax} = I_R \left(1 + 2\pi \sqrt{\frac{V_p}{2V_r}} \right)$$

Rectifier Trade-Offs

- Half-Wave Rectifier
 - + Simplest design with fewest components
 - Requires largest capacitor for a given ripple
- Full-Wave Rectifier
 - + Reduces capacitor size by $\frac{1}{2}$ relative to half-wave
 - Requires center-tapped transformer
 - PIV almost double that of half-wave
- Bridge Rectifier
 - + Reduces capacitor size by $\frac{1}{2}$ relative to half-wave
 - + Save PIV as half-wave rectifier
 - Lose two diode voltage drops in peak value